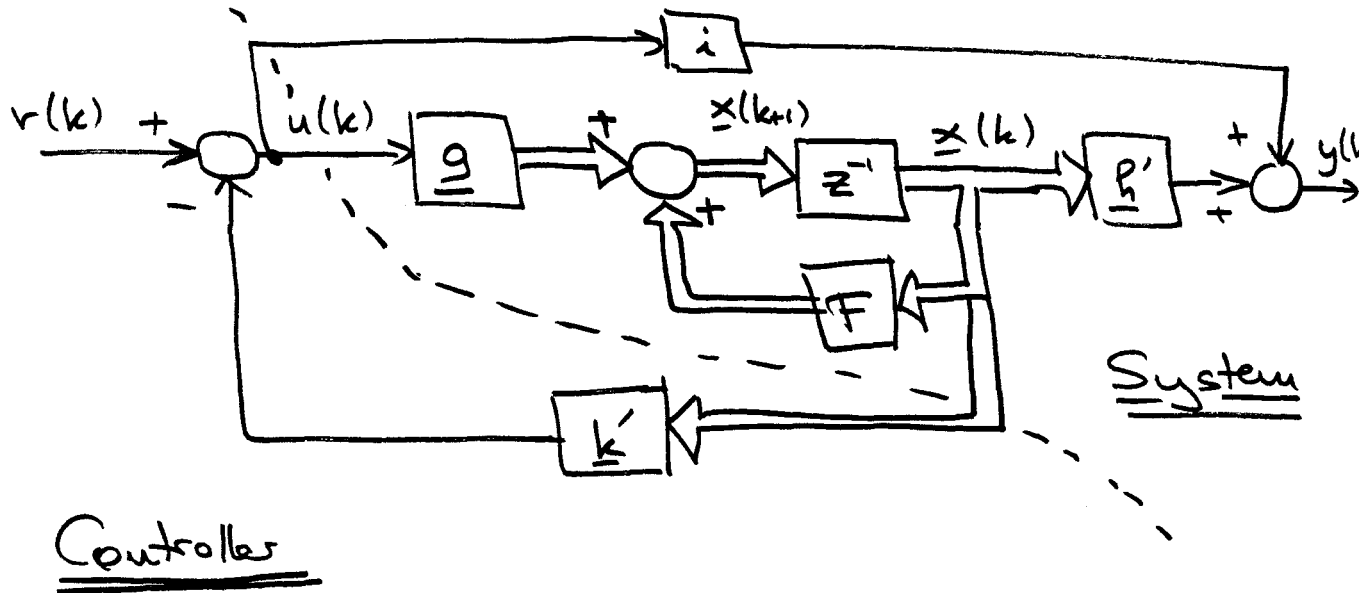


State Feedback :

Idea : As in the case of continuous systems, we can feed back a linear combination of all state variables to form the input:

$$\begin{cases} \underline{x}(k+1) = \underline{F} \cdot \underline{x}(k) + \underline{g} \cdot u(k) \\ y(k) = \underline{h}' \underline{x}(k) + i \cdot u(k) \end{cases}$$

$$\Rightarrow u(k) = -\underline{k}' \cdot \underline{x}(k) + r(k)$$



Lemma: If the plant is completely controllable, $\Rightarrow$ the poles of the closed-loop system can be selected freely.

Proof (By construction of an algorithm)

- If the system is controllable, $\Rightarrow$ we can bring it to controller-canonical form.

$$\hat{\underline{F}} = \begin{bmatrix} & & & & \\ & & & & \\ & & & & \\ & & & & \\ -a_0 & -a_1 & \dots & -a_{n-1} & \end{bmatrix} \quad \hat{\underline{g}} = \begin{bmatrix} 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix} \quad \hat{\underline{p}}_k = \begin{bmatrix} \hat{k}_1 \\ \hat{k}_2 \\ \vdots \\ \hat{k}_n \end{bmatrix}$$

unknown $\nearrow$

$$\underline{x}(k+1) = \hat{\underline{F}} \cdot \underline{x}(k) + \hat{\underline{g}} \cdot \left[-\hat{\underline{k}}' \underline{x}(k) + r(k) \right]$$

$$\Rightarrow \underline{x}(k+1) = \underbrace{\left(\hat{\underline{F}} - \hat{\underline{g}} \hat{\underline{k}}' \right)}_{\hat{\underline{F}}_{CL}} \underline{x}(k) + \hat{\underline{g}} \cdot r(k)$$

$$\Rightarrow \hat{F}_{cl} = \hat{F} - \hat{g} \cdot \hat{k}'$$

$$\hat{g} \cdot \hat{k}' = \begin{bmatrix} \emptyset & \emptyset \\ \hat{k}_1 & \hat{k}_2 & \dots & \hat{k}_n \end{bmatrix}$$

$$\Rightarrow \hat{F}_{cl} = \begin{bmatrix} \emptyset & \emptyset & \emptyset & \emptyset \\ \emptyset & \emptyset & \emptyset & \emptyset \\ \vdots & \vdots & \vdots & \vdots \\ -(a_0 + \hat{k}_1) & -(a_1 + \hat{k}_2) & \dots & -(a_{n-1} + \hat{k}_n) \end{bmatrix}$$

$\Rightarrow$ again in controller-canonical form

Example:

$$G(z) = \frac{z^2}{z^3 - 6z^2 + 11z - 6}$$

$$Q(z) = z^3 - 6z^2 + 11z - 6 = (z-1)(z-2)(z-3)$$

$\Rightarrow$ instable

We want the closed-loop poles at:

$$\left| \begin{array}{l} \lambda_1 = 1 \\ \lambda_{2,3} = 0.5 \pm 0.5j \end{array} \right|$$

$$\Rightarrow Q_{CL}(z) = (z-1)(z-0.5+0.5j)(z-0.5-0.5j) \\ = z^3 - 2z^2 + 1.5z - 0.5$$

$$F = \begin{bmatrix} \phi & 1 & \phi \\ \phi & \phi & 1 \\ 6 & -11 & 6 \end{bmatrix} = \begin{bmatrix} \phi & 1 & \phi \\ \phi & \phi & 1 \\ -a_0 & -a_1 & -a_2 \end{bmatrix}$$

$$F_{CL} = \begin{bmatrix} \phi & 1 & \phi \\ \phi & \phi & 1 \\ \phi.5 & -1.5 & 2 \end{bmatrix} = \begin{bmatrix} \phi & 1 & \phi \\ \phi & \phi & 1 \\ -(a_0 + \hat{k}_1) & -(a_1 + \hat{k}_2) & -(a_2 + \hat{k}_3) \end{bmatrix}$$

$$\Rightarrow a_0 = -6 \quad ; \quad a_0 + \hat{k}_1 = -0.5$$

$$\Rightarrow \underline{\underline{\hat{k}_1}} = -0.5 + 6 = \underline{\underline{5.5}}$$

$$a_1 = 11 \quad ; \quad a_1 + \hat{k}_2 = 1.5$$

$$\Rightarrow \underline{\underline{\hat{k}_2}} = \underline{\underline{-9.5}}$$

$$a_2 = -6 \quad ; \quad a_2 + \hat{k}_3 = -2$$

$$\Rightarrow \underline{\underline{\hat{k}_3}} = \underline{\underline{4}}$$

$$\Rightarrow \underline{\underline{\hat{k}' = [5.5 \quad -9.5 \quad 4]}}$$

will place the poles where I want them to be.

⇒ The controllable poles of a system can be placed freely by state feedback. This is called the pole placement or pole assignment problem.

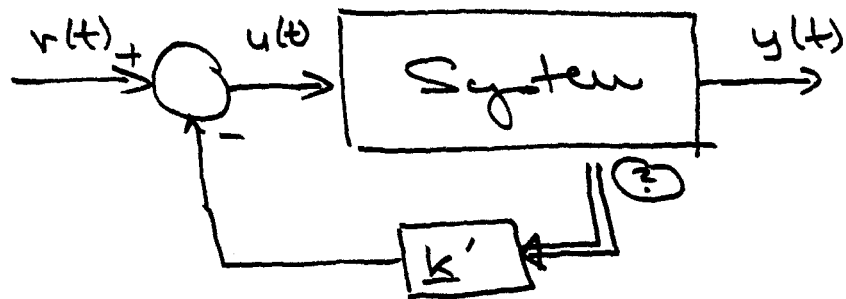
⇒ The uncontrollable poles cannot be affected at all by state feedback.

⇒ Also the zeroes remain the same. if no direct coupling.

Design of Observers.

- a) Problem: We have seen that and how we can design a state feedback to place controllable poles wherever we want them to be.

Unfortunately in a real system, what we can measure are the outputs and not the states.



$\Rightarrow$ We need output feedback.

$$\left| \begin{array}{l} \underline{x}(k+1) = F \underline{x}(k) + G \underline{u}(k) \\ \underline{y}(k) = H \underline{x}(k) + I \underline{u}(k) \end{array} \right|$$

If H is square ($p=n$) and non-singular:

$$\Rightarrow \hat{\underline{x}}(k) = H^{-1} (\underline{y}(k) - I \underline{u}(k))$$

will be a perfect observer.

However, this case is rare. E.g. our SISO-system:

$$\left| \begin{array}{l} \underline{x}(k+1) = F \underline{x}(k) + g u(k) \\ y(k) = h' \underline{x}(k) + i u(k) \end{array} \right|$$

will not satisfy the condition $p=n$ except for first-order systems.

$\Rightarrow$ We need something better.

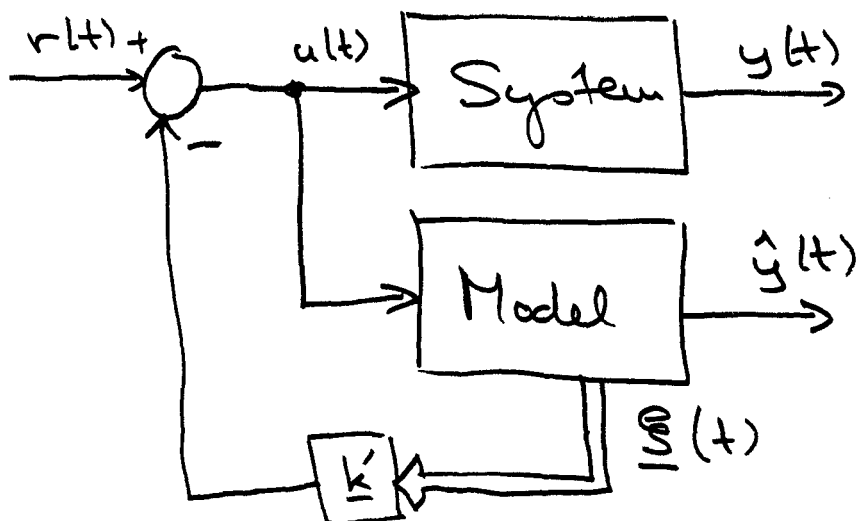
Idea: Create a model of the system:

$$\left| \begin{array}{l} \underline{\underline{\xi}}(k+1) = \underline{\underline{F}} \cdot \underline{\underline{\xi}}(k) + \underline{\underline{g}} \cdot u(k) \\ \hat{y}(k) = \underline{\underline{h}}' \cdot \underline{\underline{\xi}}(k) + i \cdot u(k) \end{array} \right|$$

If the system matrices and the initial conditions are the same

$$\Rightarrow \underline{\underline{\xi}}(k) \equiv \underline{x}(k)$$

is an "observe" for $\underline{x}(k)$.



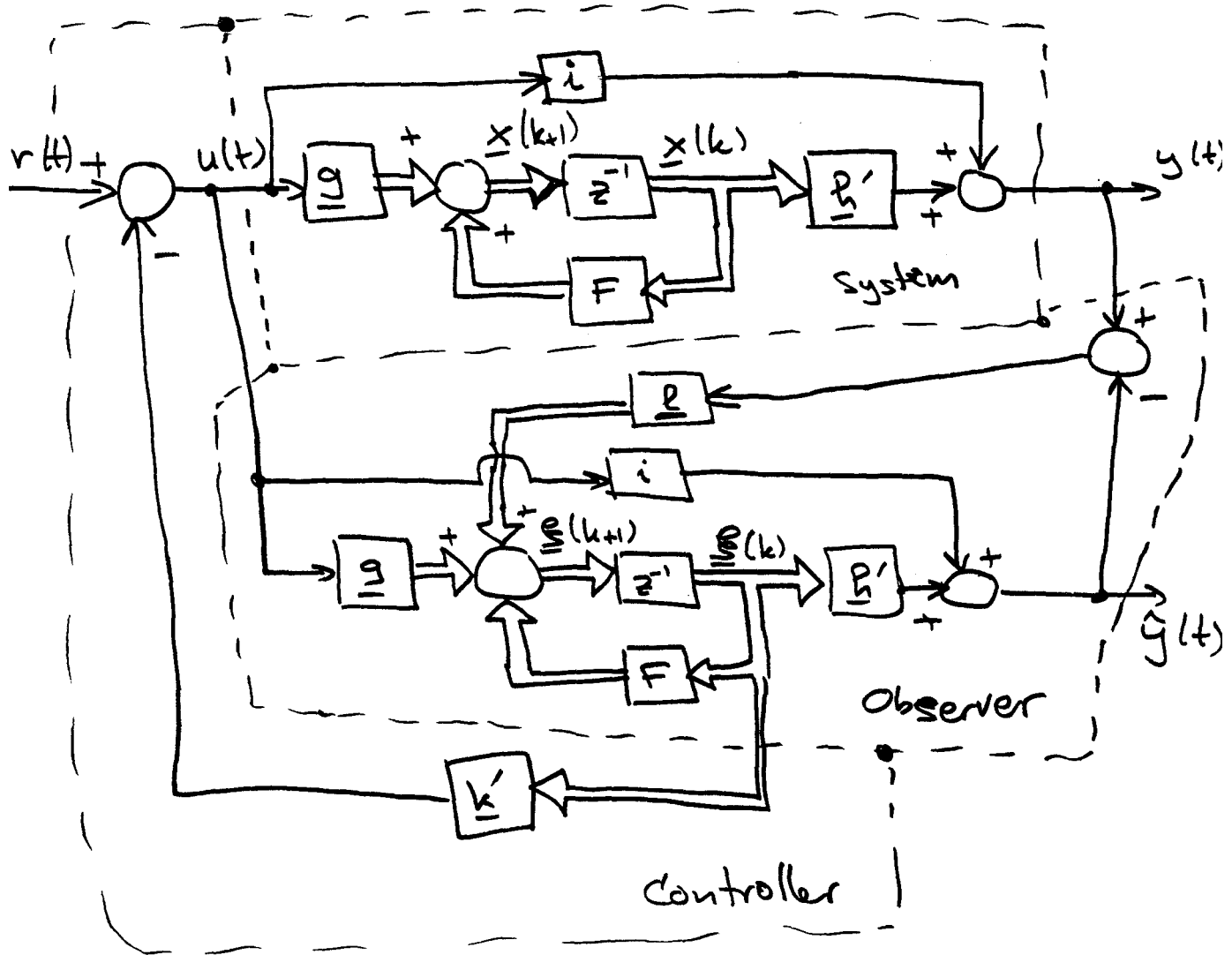
Of course, the smallest disturbance will make $\underline{\underline{e}}(k)$ drift away from $\underline{x}(k)$.

$\Rightarrow$ We need to ensure that:

$$\underline{\underline{e}}(k) = \underline{x}(k) - \underline{\underline{e}}(k) \rightarrow 0$$

as time goes to infinity.

Idea: Create a second "control"-loop to make $\underline{\underline{e}}(k)$ track $\underline{x}(k)$ even if the initial conditions are different.



$$\left| \begin{array}{l} \underline{x}(k+1) = \underline{F} \cdot \underline{x}(k) + \underline{g} \cdot u(k) \\ y(k) = \underline{P}' \cdot \underline{x}(k) + \underline{i} \cdot u(k) \end{array} \right| \quad \text{System}$$

$$\left| \begin{array}{l} \underline{\hat{x}}(k+1) = \underline{F} \cdot \underline{\hat{x}}(k) + \underline{g} u(k) + \underline{L} (y(k) - \hat{y}(k)) \\ \hat{y}(k) = \underline{P}' \cdot \underline{\hat{x}}(k) + \underline{i} \cdot u(k) \end{array} \right| \quad \text{Observer}$$

$$\left| u(k) = r(k) - \underline{K}' \cdot \underline{\hat{x}}(k) \right| \quad \text{Controller}$$

Proof that $\underline{e}(k) \rightarrow \emptyset$:

$$\begin{aligned}\underline{e}(k+1) &= \underline{x}(k+1) - \underline{z}(k+1) = F \cdot \underline{x}(k) + \underline{g} u(k) \\ &\quad - F \underline{z}(k) - \underline{g} u(k) - \underline{L} (y(k) - \hat{y}(k))\end{aligned}$$

$$\begin{aligned}\Rightarrow \underline{e}(k+1) &= F(\underline{x}(k) - \underline{z}(k)) - \underline{L} (\underline{h}' \underline{x}(k) + i u(k) \\ &\quad - \underline{h}' \underline{z}(k) - i u(k))\end{aligned}$$

$$= F \underline{e}(k) - \underline{L} \underline{h}' (\underline{x}(k) - \underline{z}(k))$$

$$\Rightarrow \boxed{\underline{e}(k+1) = (F - \underline{L} \underline{h}') \underline{e}(k)}$$

$\lim_{k \rightarrow \infty} \underline{e}(k) \rightarrow \emptyset$ iff $(F - \underline{L} \underline{h}')$ is stable.

Lemma: The poles of $(F - \underline{L}\underline{E}')$ can be chosen freely as long as the system is completely observable.

Proof (by construction)

- Bring the system into observer-canonical form.

$$\hat{F} = \begin{bmatrix} \diagup & \phi & -a_n \\ & \ddots & \vdots \\ \phi & & -a_1 \end{bmatrix} \quad \hat{g} = \begin{bmatrix} b_n \\ b_{n-1} \\ \vdots \\ b_1 \end{bmatrix} \quad \hat{e} = \begin{bmatrix} \hat{e}_1 \\ \hat{e}_2 \\ \vdots \\ \hat{e}_n \end{bmatrix}$$

$$\hat{h}' = [\phi \dots \phi \ 1]$$

$$\Rightarrow \hat{e} \hat{h}' = \begin{bmatrix} \hat{e}_1 \\ \hat{e}_2 \\ \vdots \\ \hat{e}_n \end{bmatrix}$$

$$\Rightarrow (\hat{F} - \hat{e} \hat{h}') = \begin{bmatrix} \diagup & \phi & -(a_n + \hat{e}_1) \\ & \ddots & \vdots \\ \phi & & -(a_1 + \hat{e}_n) \end{bmatrix}$$

$\Rightarrow$ yields one equation for each of the $\hat{l}_i$ q.e.d.

This looks very similar to the controller design. Indeed, if the "observer"-design is done on the dual system:

$$\left| \begin{array}{l} \overline{F} \rightarrow \overline{F}' \\ \overline{g} \rightarrow \overline{g}' \\ \overline{h} \rightarrow \overline{h}' \\ \overline{i} \rightarrow \overline{i}' \end{array} \right|$$

$$\Rightarrow (\overline{F}' - \underline{\overline{h}} \cdot \underline{\overline{h}}') \equiv (\overline{F} - \underline{\overline{g}} \underline{\overline{h}}')$$

pole placement problem.

$\Rightarrow$ The observer-problem and the pole-placement-problem are

Lemma: The observer modes are all uncontrollable.

Proof: System:
$$\begin{cases} \underline{x}(k+1) = \underline{F} \underline{x}(k) + \underline{g} u(k) \\ y(k) = \underline{h}' \underline{x}(k) + i u(k) \end{cases}$$

Observer:
$$\begin{cases} \underline{\xi}(k+1) = \underline{F} \underline{\xi}(k) + \underline{g} u(k) + \underline{l}(y(k) - \hat{y}(k)) \\ \hat{y}(k) = \underline{h}' \underline{\xi}(k) + i u(k) \end{cases}$$

Controller:
$$u(k) = r(k) - \underline{k}' \underline{\xi}(k)$$

Let us choose the following state vector of our overall system:

$$\underline{z}(k) = \begin{bmatrix} \underline{x}(k) \\ \underline{e}(k) \end{bmatrix}$$

where: $\underline{e}(k) = \underline{x}(k) - \underline{\xi}(k)$

We know already that:

$$\underline{e}(k+1) = (\underline{F} - \underline{l} \underline{h}') \cdot \underline{e}(k)$$

$$\underline{x}(k+1) = \underline{F} \cdot \underline{x}(k) + \underline{g} (r(k) - \underline{k}' \underline{e}(k))$$

$$\underline{e}(k) = \underline{x}(k) - \underline{e}(k)$$

$$\Rightarrow \underline{x}(k+1) = \underline{F} \cdot \underline{x}(k) + \underline{g} r(k) - \underline{g} \underline{k}' \underline{x}(k) + \underline{g} \underline{k}' \underline{e}(k)$$

$$\Rightarrow \underline{x}(k+1) = (\underline{F} - \underline{g} \underline{k}') \underline{x}(k) + \underline{g} \underline{k}' \underline{e}(k) + \underline{g} \cdot r(k)$$

$$\Rightarrow \begin{cases} \underline{y}(k+1) = \begin{bmatrix} (\underline{F} - \underline{g} \underline{k}') & \underline{g} \underline{k}' \\ \Phi & (\underline{F} - \underline{g} \underline{k}') \end{bmatrix} \underline{y}(k) + \begin{bmatrix} \underline{g} \\ \Phi \end{bmatrix} \cdot r(k) \\ y(k) = \begin{bmatrix} (\underline{p}' - i \underline{k}') & i \underline{k}' \end{bmatrix} \underline{y}(k) + \begin{bmatrix} i \end{bmatrix} \cdot r(k) \end{cases}$$

$\Rightarrow$ From the structure, it becomes obvious that:

(1) the $\underline{F}_{CL}$ -matrix is block-triangular

$$\Rightarrow \text{eig}(\underline{F}_{CL}) = \underbrace{\{ \text{eig}(\underline{F} - \underline{g} \underline{k}') \}}_{\text{controller modes}} ; \underbrace{\{ \text{eig}(\underline{F} - \underline{g} \underline{k}') \}}_{\text{observer modes}}$$

(2) the observer-modes are uncontrollable.

Lemma: The particular set of state variables chosen e.g. for the control (feedback) is immaterial.

Proof (trivial): As the observer is only fed by inputs and outputs, the actual states do not appear explicitly. Thus, it is perfectly okay to write:

System:
$$\begin{cases} \underline{x}(k+1) = \underline{F} \cdot \underline{x}(k) + \underline{g} \cdot u(k) \\ y(k) = \underline{h}' \cdot \underline{x}(k) + i \cdot u(k) \end{cases}$$

Observer:
$$\begin{cases} \underline{e}(k+1) = \hat{\underline{F}} \cdot \underline{e}(k) + \hat{\underline{g}} \cdot u(k) + \hat{\underline{e}}(y - \hat{y}) \\ \hat{y}(k) = \hat{\underline{h}}' \cdot \underline{e}(k) + i \cdot u(k) \end{cases}$$

Controller:
$$u(k) = r(k) - \hat{\underline{k}}' \cdot \underline{e}(k)$$

where:
$$\begin{cases} \hat{\underline{F}} = \underline{T} \cdot \underline{F} \cdot \underline{T}^{-1} \\ \hat{\underline{g}} = \underline{T} \cdot \underline{g} \\ \hat{\underline{h}}' = \underline{h}' \cdot \underline{T}^{-1} \end{cases}$$

that is: we can choose a base representation, and then transform everything into this one representation.

E.g. We might choose the controller-canonical form as a base representation

$\Rightarrow$ The $\underline{K}'$ -vector found earlier will be correct as it assumes the $\underline{E}(k)$ in this form.

$\Rightarrow$ The $\hat{\underline{P}}$ -vector, however, will be incorrect, as it assumes the $\hat{\underline{E}}(k)$ in observer-canonical form.

$\Rightarrow$ We need to transform it back to controller-canonical form.

Let us assume, we were in the "beginning" in controller - canonical form ($\underline{x}$ are state-variables in controller - canonical form)

$$\Rightarrow \underline{z} = T \cdot \underline{x}$$

is the transformation that gets us into observer - canonical form.

After this transformation, we can build an observer for $\underline{z}$:

$$\underline{z}(k+1) = \hat{F} \cdot \underline{z}(k) + \hat{g} u(k) + \hat{L} (y(k) - \hat{y}(k))$$

Obviously, if $\underline{y}$ observes $\underline{z}$

$$\Rightarrow \underline{z} = T^{-1} \cdot \underline{y} \quad \text{observes } \underline{x}$$

$$\Rightarrow \underline{y}(k) = T \cdot \underline{z}(k)$$

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$$\Rightarrow T \underline{\underline{x}}(k+1) = \hat{F} \cdot T \underline{\underline{x}}(k) + \hat{g} u(k) + \hat{\ell} (y(k) - \hat{y}(k))$$

$$\Rightarrow \underline{\underline{x}}(k+1) = \underbrace{T^{-1} \cdot \hat{F} \cdot T}_{\underline{\underline{F}}} \underline{\underline{x}}(k) + \underbrace{T^{-1} \hat{g}}_{\underline{\underline{g}}} u(k) + T^{-1} \hat{\ell} (y(k) - \hat{y}(k))$$

is an observer for $\underline{\underline{x}}(k)$

$$\Rightarrow \underline{\underline{x}}(k+1) = \underline{\underline{F}} \cdot \underline{\underline{x}}(k) + \underline{\underline{g}} u(k) + \underline{\underline{\ell}} (y(k) - \hat{y}(k))$$

$$\Rightarrow \underline{\underline{\ell}} = T^{-1} \hat{\ell}$$

is the back-transformation into the original (controller - canonical) coordinates.