The Theoretical Underpinnings of the Bond Graph Methodology

- In this lecture, we shall look more closely at the theoretical underpinnings of the bond graph methodology: the four base variables, the properties of capacitive and inductive storage elements, and the duality principle.
- We shall also introduce the two types of energy transducers: the transformers and the gyrators, and we shall look at hydraulic bond graphs.



Table of Contents

- The four base variables of the bond graph methodology
- <u>Properties of storage elements</u>
- Hydraulic bond graphs
- Energy transducers
- <u>Electromechanical systems</u>
- The duality principle
- The diamond rule





The Four Base Variables of the Bond Graph Methodology

• Beside from the two adjugate variables *e* and *f*, there are two additional physical quantities that play an important role in the bond graph methodology:

<u>Generalized Momentum:</u>

$$p = \int e \cdot dt$$

Generalized Position:

$$q = \int f \cdot dt$$

October 11, 2012







Relations Between the Base Variables



<u>Resistor:</u>	e = R(f)
<u>Capacity:</u>	q = C(e)
<u>Inductivity:</u>	p = I(f)
	<u>ሱ</u>

Arbitrarily non-linear functions in 1st and 3rd quadrants

 \Rightarrow There cannot exist other storage elements besides C and I.





Linear Storage Elements

General capacitive equation:

$$q = C(e)$$

<u>Linear capacitive equation:</u>

$$q = C \cdot e$$

<u>Linear capacitive equation</u> <u>differentiated:</u>

$$f = C \cdot \frac{de}{dt}$$

"Normal" capacitive equation, as hitherto commonly encountered.

October 11, 2012



	Effort	Flow	Generalized Momentum	Generalized Position
	е	f	р	q
Electrical Circuits	Voltage <i>u</i> (V)	Current <i>i</i> (A)	Magnetic Flux	Charge q (A·sec)
Translational Systems	Force F (N)	Velocity v (m / sec)	Momentum M (N·sec)	Position x (m)
Rotational Systems	Torque T (N·m)	Angular Velocity ω (rad / sec)	Torsion T (N·m·sec)	Angle φ (rad)
Hydraulic Systems	Pressure <i>p</i> (N / m ²)	Volume Flow $q \pmod{(\text{m}^3 / \text{sec})}$	Pressure Momentum Γ (N·sec / m ²)	Volume V (m ³)
Chemical Systems	Chem. Potential μ (J / mol)	Molar Flow ν (mol/sec)	-	Number of Moles <i>n</i> (mol)
Thermodynamic Systems	Temperature T (K)	Entropy Flow S' (W / K)	-	Entropy S (J / K)

October 11, 2012

© Prof. Dr. François E. Cellier

Start Presentation





• In hydrology, the two adjugate variables are the *pressure p* and the *volume flow q*. Here, the pressure is considered the potential variable, whereas the volume flow plays the role of the flow variable.

$$P_{hydr} = p \cdot q$$

$$[W] = [N/m^{2}] \cdot [m^{3}/s]$$
$$= kg \cdot m^{-1} \cdot s^{-2}] \cdot [m^{3} \cdot s^{-1}]$$
$$= [kg \cdot m^{2} \cdot s^{-3}]$$

• The *capacitive storage* describes the compressibility of the fluid as a function of the pressure, whereas the *inductive storage* models the inertia of the fluid in motion.

Eidgenössische Technische Hochschule Zürich Swiss Federal Institute of Technology Zurich



Hydraulic Bond Graphs II

Compression:



Laminar Flow:

$$\begin{array}{c} P_2 \\ = k \cdot \Delta p \\ = k \cdot (p_1 - p_2) \end{array} \begin{array}{c} \Delta p \\ \hline q \end{array} \\ R : 1/k \end{array}$$

Turbulent Flow:

$$p_1 \longrightarrow p_2$$

$$\frac{\Delta p}{q} - G^{\text{Hydro}} = k \cdot \text{sign}(\Delta p) \cdot \sqrt{|\Delta p|}$$

October 11, 2012

*p*₁

Prof. Dr. François E. Cellier \bigcirc

q



Energy Conversion

- Beside from the elements that have been considered so far to describe the *storage of energy* (*C* and *I*) as well as its *dissipation (conversion to heat)* (*R*), two additional elements are needed, which describe the general *energy conversion*, namely the *Transformer* and the *Gyrator*.
- Whereas resistors describe the *irreversible conversion of free energy into heat*, transformers and gyrators are used to model *reversible energy conversion phenomena* between identical or different forms of energy.



Transformers



ransformation:
$$e_1 = m \cdot e_2$$
(1)nergy Conservation: $e_1 \cdot f_1 = e_2 \cdot f_2$ (2) $\implies (m \cdot e_2) \cdot f_1 = e_2 \cdot f_2$ (3) $\implies f_2 = m \cdot f_1$ (4)

⇒ The transformer may either be described by means of equations (1) and (2) or using equations (1) and (4).

October 11, 2012



The Causality of the Transformer

$$\begin{vmatrix} e_{1} & \mathbf{TF} & e_{2} \\ f_{1} & \mathbf{TF} & f_{2} \end{vmatrix} \qquad e_{1} = m \cdot e_{2} \\ f_{2} = m \cdot f_{1} \end{vmatrix}$$

$$\frac{e_{1}}{f_{1}} & \mathbf{TF} & \frac{e_{2}}{f_{2}} & e_{2} = e_{1}/m \\ f_{1} = f_{2}/m \end{vmatrix}$$

 \Rightarrow As we have exactly one equation for the effort and another for the flow, it is mandatory that the transformer compute one effort variable and one flow variable. Hence there is one causality stroke at the TF element.

JZ

JI

October 11, 2012

Prof. Dr. François E. Cellier (\mathbf{C})





Examples of Transformers



October 11, 2012



Gyrators





⇒ The gyrator may either be described by means of equations (1) and (2) or using equations (1) and (4).

October 11, 2012





The Causality of the Gyrator

$$\begin{array}{c|c} e_1 \\ \hline f_1 \\ \hline f_1 \\ \end{array} \begin{array}{c} e_2 \\ \hline f_2 \\ \end{array} \begin{array}{c} e_1 = r \cdot f_2 \\ e_2 = r \cdot f_1 \end{array}$$

$$\begin{array}{c|c} \mathbf{e}_1 & \mathbf{G}_2 \\ \hline \mathbf{f}_1 & \mathbf{G}_r \mathbf{Y} \\ \hline \mathbf{f}_2 \end{array} \qquad \begin{array}{c|c} \mathbf{f}_2 = \mathbf{e}_2 \\ \mathbf{f}_1 = \mathbf{e}_2 \\ \hline \mathbf{f}_1 = \mathbf{e}_2 \end{array}$$

⇒ As we must compute one equation to the left, the other to the right of the gyrator, the equations may either be solved for the two effort variables or for the two flow variables.

October 11, 2012

© Prof. Dr. François E. Cellier

Start Presentation



Examples of Gyrators



The DC motor generates a torque τ_m proportional to the armature current i_a , whereas the resulting induced Voltage u_i is proportional to the angular velocity \mathcal{O}_m .

October 11, 2012





Example of an Electromechanical System



October 11, 2012



The Duality Principle

- It is always possible to *"dualize"* a bond graph by switching the definitions of the effort and flow variables.
- In the process of dualization, effort sources become flow sources, capacities turn into inductors, resistors are converted to conductors, and vice-versa.
- Transformers and gyrators remain the same, but their transformation values are inverted in the process.
- The two junctions exchange their type.
- The causality strokes move to the other end of each bond.



1st Example



The two bond graphs produce identical simulation results.

October 11, 2012

© Prof. Dr. François E. Cellier

Start Presentation







Partial Dualization

- It is always possible to dualize bond graphs only in parts.
 - It is particularly easy to partially dualize a bond graph at the transformers and gyrators. The two conversion elements thereby simply exchange their types.
 - For example, it may make sense to only dualize the mechanical side of an electromechanical bond graph, whereas the electrical side is left unchanged.
 - However, it is also possible to dualize the bond graph at any bond. Thereby, the "twisted" bond is turned into a gyrator with a gyration of *r*=1.
 - Such a gyrator is often referred to as *symplectic gyrator* in the bond graph literature.



Manipulation of Bond Graphs

- Any physical system with concentrated parameters can be described by a bond graph.
- However, the bond graph representation is not unique, i.e., several different-looking bond graphs may represent identical equation systems.
- One type of ambiguity has already been introduced: the *dualization*.
- However, there exist other classes of ambiguities that cannot be explained by dualization.







October 11, 2012

© Prof. Dr. François E. Cellier

Start Presentation



References

 Cellier, F.E. (1991), <u>Continuous System Modeling</u>, Springer-Verlag, New York, <u>Chapter 7</u>.

October 11, 2012



