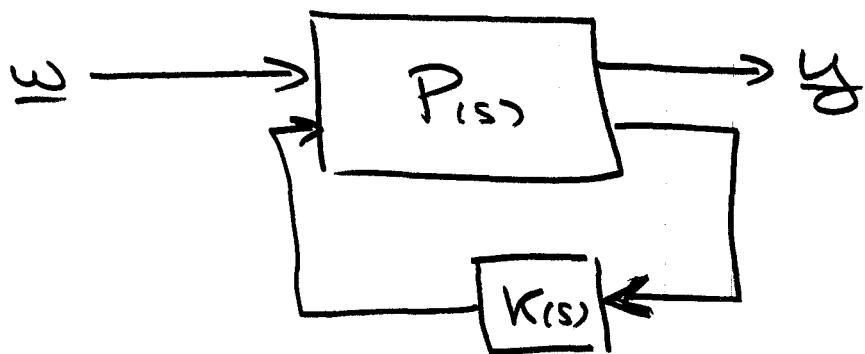


This is the robustness problem.

### Linear Fractional Transforms:

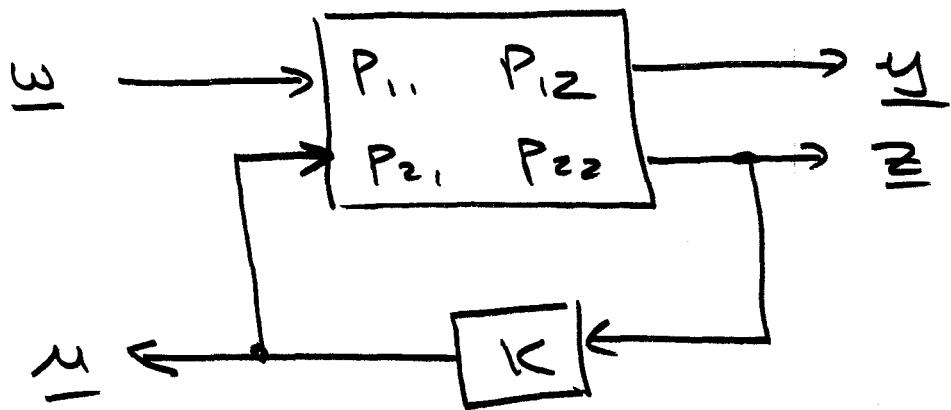
Given :



What is the transfer function  
from  $W \rightarrow Y$  ?

$$P_{(s)} = \begin{bmatrix} P_{11}(s) & P_{12}(s) \\ P_{21}(s) & P_{22}(s) \end{bmatrix}$$

$P_{ij}(s)$  can still be  
multivariable !



$$U_1 = P_{11} \cdot E_1 + P_{12} \cdot U$$

$$U_2 = P_{21} \cdot E_2 + P_{22} \cdot U$$

$$U = K \cdot U$$

$$\Rightarrow U = K \cdot U = K P_{11} \cdot E_1 + K P_{12} \cdot U$$

$$\Rightarrow [I - K P_{12}] U = K P_{11} \cdot E_1$$

$$\Rightarrow U = [I - K P_{12}]^{-1} K P_{11} \cdot E_1$$

$$\Rightarrow U = \left[ P_{11} + P_{12} [I - K P_{12}]^{-1} K P_{11} \right] E_1$$

$$\Rightarrow F_e(P, K) = P_{11} + P_{12} [I - K P_{12}]^{-1} K P_{11}$$

500 SHEETS, FILLER, 5 SQUARE  
50 SHEETS, EYE, TAPE, 5 SQUARE  
100 SHEETS, EYE, ASH, 5 SQUARE  
200 SHEETS, EYESASH, 5 SQUARE  
100 RECYCLED, WHITE, 5 SQUARE  
200 RECYCLED, WHITE, 5 SQUARE  
Made in U.S.A.

Fine National's Brand

$\Sigma$ :

$$\underline{\Xi} = P_{21} \cdot \underline{w} + P_{22} K \cdot \underline{z}$$

$$\Rightarrow [I - P_{22} K] \underline{\Xi} = P_{21} \underline{w}$$

$$\Rightarrow \underline{\Xi} = [I - P_{22} K]^{-1} P_{21} \underline{w}$$

$$\Rightarrow \underline{y} = K \underline{\Xi} = K [I - P_{22} K]^{-1} P_{21} \underline{w}$$

$$\Rightarrow \underline{y} = \left[ P_{11} + P_{12} K [I - P_{22} K]^{-1} P_{21} \right] \underline{w}$$

$$\Rightarrow \underline{f}_e(P, K) = P_{11} + P_{12} K [I - P_{22} K]^{-1} P_{21}$$

$\underline{f}_e(P, K)$  is the lower linear fractional transform of  $P$  fed back by  $K$ .

13-702 ECO SHEETS, FILLER, 5 SQUARE  
42-391 50 SHEETS, EYE-FADED, 5 SQUARE  
42-392 100 SHEETS, EYE-FADED, 5 SQUARE  
42-399 200 SHEETS, EYE-FADED, 5 SQUARE  
42-392 100 RECYCLED, WHITE, 5 SQUARE  
42-399 200 RECYCLED, WHITE, 5 SQUARE  
Made in U.S.A.



In the time domain:

$$P(s) = \left[ \begin{array}{c|cc} A_p & B_{p1} & B_{p2} \\ \hline C_{p1} & D_{p11} & D_{p12} \\ C_{p2} & D_{p21} & D_{p22} \end{array} \right]$$

$$K(s) = \left[ \begin{array}{c|c} A_k & B_k \\ \hline C_k & D_k \end{array} \right]$$

$$\begin{aligned} \dot{x}_p &= A_p x_p + B_{p1} \psi + B_{p2} \underline{u} \\ \dot{\psi} &= C_{p1} x_p + D_{p11} \psi + D_{p12} \underline{u} \\ \underline{u} &= C_{p2} x_p + D_{p21} \psi + D_{p22} \underline{u} \\ \dot{x}_k &= A_k x_k + B_k \underline{u} \\ \underline{u} &= C_k x_k + D_k \underline{z} \end{aligned}$$

$$\underline{u} = C_k x_k + D_k C_{p2} x_p + D_k D_{p21} \psi + D_k D_{p22} \underline{u}$$

$$\Rightarrow \underbrace{(I - D_k D_{p22})}_{DD} \underline{u} = C_k x_k + D_k C_{p2} x_p + D_k D_{p21} \psi$$

$$\Rightarrow \underline{u} = DD^{-1} D_k C_{p2} x_p + DD^{-1} D_k C_k x_k + DD^{-1} D_k D_{p21} \psi$$

$$\Rightarrow \dot{X}_P = [A_P + B_{P_2} \cdot D \bar{D}^{-1} D_K C_{P_2}] X_P + [B_{P_2} \cdot D \bar{D}^{-1} C_K] X_K \\ + [B_{P_1} + B_{P_2} \cdot D \bar{D}^{-1} D_{Kc} D_{P_2}] \underline{\omega}$$

$$\dot{X}_K = B_K C_{P_2} X_P + A_K X_K + B_K D_{P_2} \underline{\omega} + B_{Kc} D_{P_2} \underline{\omega}$$

$$\Rightarrow \dot{X}_K = [B_K C_{P_2} + B_K D_{P_2} \cdot D \bar{D}^{-1} D_K C_{P_2}] X_P \\ + [A_K + B_K D_{P_2} \cdot D \bar{D}^{-1} C_K] X_K \\ + [B_{Kc} D_{P_2} + B_{Kc} D_{P_2} \cdot D \bar{D}^{-1} D_K D_{P_2}] \underline{\omega}$$

$$Y = [C_{P_1} + D_{P_{12}} \cdot D \bar{D}^{-1} D_K C_{P_2}] X_P + [D_{P_{12}} \cdot D \bar{D}^{-1} C_K] X_K \\ + [D_{P_{11}} + D_{P_{12}} \cdot D \bar{D}^{-1} D_K D_{P_2}] \underline{\omega}$$

$$\Rightarrow F_2(P, K) = \frac{\begin{bmatrix} (A_P + B_{P_2} D \bar{D}^{-1} D_K C_{P_2}) & (B_{P_2} D \bar{D}^{-1} C_K) \\ (D_K C_{P_2} + B_K D_{P_2} \cdot D \bar{D}^{-1} D_K C_{P_2}) & (A_K + B_{Kc} D_{P_2} \cdot D \bar{D}^{-1} C_K) \end{bmatrix}}{\begin{bmatrix} (C_{P_1} + D_{P_{12}} D \bar{D}^{-1} D_K C_{P_2}) & (D_{P_{12}} D \bar{D}^{-1} C_K) \end{bmatrix}}$$

$$\frac{\begin{bmatrix} (B_{P_1} + B_{P_2} D \bar{D}^{-1} D_K D_{P_2}) \\ (B_{Kc} D_{P_2} + B_K D_{P_2} \cdot D \bar{D}^{-1} D_{Kc} D_{P_2}) \end{bmatrix}}{(D_{P_{11}} + D_{P_{12}} D \bar{D}^{-1} D_K D_{P_2})}$$

13-762 500 SHEETS, HILGER, 5" SQUARE  
42-331 50 SHEETS, EYE-EASE, 5" SQUARE  
42-332 100 SHEETS, EYE-EASE, 5" SQUARE  
200-SHEET EYE-EASE, 5" SQUARE  
42-382 100 RECYCLED, WHITE, 5" SQUARE  
42-389 200 RECYCLED, WHITE, 5" SQUARE

National® Brand  
Made in U.S.A.

$$P_p(s) \cdot \underline{x}_p(t) = Q_{P_1}(s) \cdot \underline{w}(t) + Q_{P_2}(s) \cdot \underline{u}(t)$$

$$\underline{y}(t) = R_{P_1}(s) \cdot \underline{x}_p(t) + W_{P_1}(s) \cdot \underline{w}(t) + W_{P_2}(s) \cdot \underline{u}(t)$$

$$\underline{z}(t) = R_{P_2}(s) \cdot \underline{x}_p(t) + W_{P_2}(s) \cdot \underline{w}(t) + W_{P_2}(s) \cdot \underline{u}(t)$$

$$P_k(s) \cdot \underline{x}_k(t) = Q_k(s) \cdot \underline{z}(t)$$

$$\underline{y}(t) = R_k(s) \cdot \underline{x}_k(t) + W_k(s) \cdot \underline{z}(t)$$

$$P_p(s) \cdot \underline{x}_p(t) - Q_{P_2}(s) \cdot \underline{y}(t) = Q_{P_1}(s) \cdot \underline{w}(t)$$

$$P_k(s) \cdot \underline{x}_k(t) - Q_k(s) \cdot \underline{z}(t) = \emptyset$$

$$R_k(s) \cdot \underline{x}_k(t) - W_k(s) \cdot \underline{z}(t) + \underline{u}(t) = \emptyset$$

$$R_{P_2}(s) \cdot \underline{x}_p(t) + \underline{z}(t) - W_{P_2}(s) \cdot \underline{y}(t) = W_{P_2}(s) \cdot \underline{w}(t)$$

$$\underline{y}(t) = R_{P_1}(s) \cdot \underline{x}_p(t) + W_{P_2}(s) \cdot \underline{u}(t) + W_{P_1}(s) \cdot \underline{w}(t)$$

Let:  $\underline{\omega}(t) = \begin{bmatrix} \underline{x}_p(t) \\ \underline{x}_k(t) \\ -\underline{z}(t) \\ -\underline{u}(t) \end{bmatrix}$

13-782  
42-581 500 SHEETS FILLER 5 SQUARE  
42-582 100 SHEETS ERASER 5 SQUARE  
42-589 100 SHEETS ERASER  
42-590 100 RECYCLED WHITE 5 SQUARE  
42-593 200 RECYCLED WHITE 5 SQUARE  
National Brand  
Nestle U.S.A.

$$\Rightarrow \begin{bmatrix} P_p(s) & \emptyset & \emptyset & Q_{P_2}(s) \\ \emptyset & P_k(s) & Q_k(s) & \emptyset \\ \emptyset & -R_k(s) & W_k(s) & -I \\ -R_{P_2}(s) & \emptyset & -I & W_{P_{22}}(s) \end{bmatrix} \underline{\mathbf{w}}(t) = \begin{bmatrix} Q_{P_1}(s) \\ \emptyset \\ \emptyset \\ W_{P_{21}}(s) \end{bmatrix} w(t)$$

$$\underline{\mathbf{y}}(t) = [R_{P_1}(s) \ \emptyset \ \emptyset \ -W_{P_{12}}(s)] \underline{\mathbf{w}}(t) + [W_{P_{11}}(s)] u(t)$$

is a polynomial matrix system representation of  $f_e(P, K)$ .

$$\Rightarrow S(s) = \begin{bmatrix} P_p(s) & \emptyset & \emptyset & Q_{P_2}(s) \\ \emptyset & P_k(s) & Q_k(s) & \emptyset \\ \emptyset & -R_k(s) & W_k(s) & -I \\ -R_{P_2}(s) & \emptyset & -I & W_{P_{22}}(s) \\ R_{P_1}(s) & \emptyset & \emptyset & W_{P_{12}}(s) \end{bmatrix} \begin{bmatrix} Q_{P_1}(s) \\ \emptyset \\ \emptyset \\ W_{P_{21}}(s) \end{bmatrix}$$

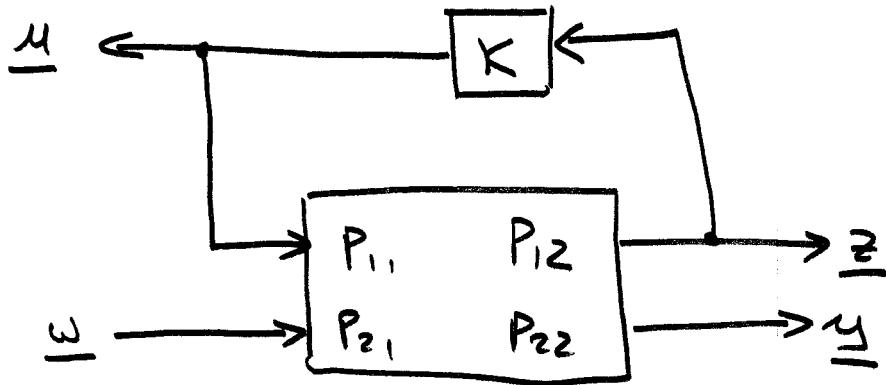


```
end,
end
if debg >= 2,
  if mG <= pK,
    disp('LFTL: Error - Incompatible number of rows/columns'),
    abort,
  end,
  if pG <= mK,
    disp('LFTL: Error - Incompatible number of rows/columns'),
    abort,
  end,
end
%
% Branch depending on the mode of the system.
%
if modG == 0,
%
% Is a state-space description
%
[Ag,Bg,Cg,Dg] = oldsyst(G);
[Ak,Bk,Ck,Dk] = oldsyst(K);
%
% Extract the four subsystems.
%
Bg1 = Bg(:,1:mG-pK);
Bg2 = Bg(:,mG-pK+1:mG);
Cg1 = Cg(1:pG-mK,:);
Cg2 = Cg(pG-mK+1:pG,:);
Dg11 = Dg(1:pG-mK,1:mG-pK);
Dg12 = Dg(1:pG-mK,mG-pK+1:mG);
Dg21 = Dg(pG-mK+1:pG,1:mG-pK);
Dg22 = Dg(pG-mK+1:pG,mG-pK+1:mG);
DkDg22 = Dk*Dg22;
DD = eye(size(DkDg22)) - DkDg22;
%
% Check whether the problem is well-posed
%
if norm(DD) < 1000*eps,
  disp('LFTL: Error - System is ill-posed'),
  abort,
  return,
end,
%
% Now compute the feedback structure
%
DDinv = inv(DD);
Bg2DDi = Bg2*DDinv;
BkDg22DDi = Bk*Dg22*DDinv;
DkCg2 = Dk*Cg2;
DkDg21 = Dk*Dg21;
Bcl1 = Bg1 + Bg2DDi*DkDg21;
Bcl2 = Bk*Dg21 + BkDg22DDi*DkDg21;
Bcl = [ Bcl1 ; Bcl2 ];
Acl11 = Ag + Bg2DDi*DkCg2;
Acl12 = Bg2DDi*Ck;
Acl21 = Bk*Cg2 + BkDg22DDi*DkCg2;
Acl22 = Ak + BkDg22DDi*Ck;
Acl = [ Acl11 , Acl12 ; Acl21 , Acl22 ];
Dg12DDi = Dg12*DDinv;
Dcl = Dg11 + Dg12DDi*DkDg21;
```

```
Ccl1 = Cg1 + Dg12DDi*DkCg2;
Ccl2 = Dg12DDi*Ck;
Ccl = [ Ccl1 , Ccl2 ];
T = newsyst(Acl,Bcl,Ccl,Dcl,stypG);
%
% Get rid of uncontrollable/unobservable modes
%
T = minreals(T);
pull,
return,
end
%
if modG == 4 | modG == 5 | modG == 6,
%
% Is a transfer function matrix
% Extract the four submatrices.
%
G11 = gget(G,1:pG-mK,1:mG-pK);
G12 = gget(G,1:pG-mK,mG-pK+1:mG);
G21 = gget(G,pG-mK+1:pG,1:mG-pK);
G22 = gget(G,pG-mK+1:pG,mG-pK+1:mG);
%
% Now compute: T = G11 + G12*K*(I - G22*K)\G21
%
Aux = multg(G22,K);
I = eyep(mK,mK,modG,logcol,stypG,domG);
Aux = sub(I,Aux);
%
% Check whether system is well-posed
%
[G2,P2] = strictprop(Aux);
ord = order(P2);
if ord == 0,
  gn = gain(P2);
  if gn == 0,
    disp('LFTL: Error - System is ill-posed'),
    abort,
    return,
  end,
end,
Aux = invg(Aux);
Aux = multg(Aux,G21);
Aux = multg(K,Aux);
Aux = multg(G12,Aux);
T = addg(G11,Aux);
%
% Get rid of uncontrollable/unobservable modes
%
T = reduceeg(T);
pull,
return,
end
%
if modG == 7 | modG == 8 | modG == 9,
%
% Is a polynomial matrix system description
%
[Pg,Qg,Rg,Wg] = pms2plm(G);
[Pk,Qk,Rk,Wk] = pms2plm(K);
%
```

```
% Extract the four subsystems
%
[nQ,mQ] = logdim(Qg);
[nR,mR] = logdim(Rg);
Qg1 = gget(Qg,1:nQ,1:mG-pK);
Qg2 = gget(Qg,1:nQ,mG-pK+1:mG);
Rg1 = gget(Rg,1:pG-mK,1:mR);
Rg2 = gget(Rg,pG-mK+1:pG,1:mR);
Wg11 = gget(Wg,1:pG-mK,1:mG-pK);
Wg12 = gget(Wg,1:pG-mK,mG-pK+1:mG);
Wg21 = gget(Wg,pG-mK+1:pG,1:mG-pK);
Wg22 = gget(Wg,pG-mK+1:pG,mG-pK+1:mG);
%
% Plug closed loop polynomial matrices together
%
[qG,qG] = logdim(Pg);
[qK,qK] = logdim(Pk);
qT = qG + qK + mK + pK;
pT = pG - mK;
mT = mG - pK;
Pcl = zerop(qT,qT,modG-6,logcol,stypG,domG);
Im = eyep(mK,mK,modG-6,logcol,stypG,domG);
Ip = eyep(pK,pK,modG-6,logcol,stypG,domG);
Pcl = put(Pcl,Pg,1:qG,1:qG);
Pcl = put(Pcl,Qg2,1:qG,qT-pK+1:qT);
Pcl = put(Pcl,Pk,qG+1:qG+qK,qG+1:qG+qK);
Pcl = put(Pcl,Qk,qG+1:qG+qK,qG+qK+1:qT-pK);
Pcl = put(Pcl,minus(Rk),qG+qK+1:qT-mK,qG+1:qG+qK);
Pcl = put(Pcl,Wk,qG+qK+1:qT-mK,qG+qK+1:qT-pK);
Pcl = put(Pcl,minus(Ip),qG+qK+1:qT-mK,qT-pK+1:qT);
Pcl = put(Pcl,minus(Rg2),qT-mK+1:qT,1:qG);
Pcl = put(Pcl,minus(Im),qT-mK+1:qT,qG+qK+1:qT-pK);
Pcl = put(Pcl,Wg22,qT-mK+1:qT,qT-pK+1:qT);
Qcl = zerop(qT,mT,modG-6,logcol,stypG,domG);
Qcl = put(Qcl,Qg1,1:qG,1:mT);
Qcl = put(Qcl,Wg21,qT-mK+1:qT,1:mT);
Rcl = zerop(pT,qT,modG-6,logcol,stypG,domG);
Rcl = put(Rcl,Rg1,1:pT,1:qG);
Rcl = put(Rcl,minus(Wg12),1:pT,qT-pK+1:qT);
Wcl = Wg11;
%
% Make a new polynomial matrix system
%
T = plm2pms(Pcl,Qcl,Rcl,Wcl);
%
% Get rid of uncontrollable/unobservable modes
%
T = minrealps(T);
pull,
return,
end
%
return
```

Analogous:



National® Brand  
13-762 500 SHEETS FILLER 5 SQUARE  
45-381 500 SHEETS FILLER 5 SQUARE  
45-382 100 SHEETS FILLER 5 SQUARE  
45-389 200 SHEETS FILLER 5 SQUARE  
45-392 100 RECYCLED WHITE 5 SQUARE  
45-393 200 RECYCLED WHITE 5 SQUARE  
Vallejo, CA

$$\left| \begin{array}{l} Z = P_{11} \cdot U + P_{12} \cdot E \\ Y = P_{21} \cdot U + P_{22} \cdot E \\ U = K \cdot Z \end{array} \right|$$

$$\Rightarrow U = K \cdot Z = K \cdot P_{11} \cdot U + K \cdot P_{12} \cdot E$$

$$\Rightarrow [I - K \cdot P_{11}] U = K \cdot P_{12} E$$

$$\Rightarrow U = [I - K \cdot P_{11}]^{-1} \cdot K \cdot P_{12} E$$

$$\Rightarrow U = [P_{22} + P_{21} \cdot [I - K \cdot P_{11}]^{-1} \cdot K \cdot P_{12}] E$$

$$\Rightarrow f_u(P, K) = P_{22} + P_{21} [I - K \cdot P_{11}]^{-1} \cdot K \cdot P_{12}$$

or:

$$\underline{z} = P_{11} \cdot \underline{u} + P_{12} \cdot \underline{\omega}$$

$$= P_{11} \cdot K \cdot \underline{z} + P_{12} \cdot \underline{\omega}$$

$$\Rightarrow [I - P_{11} \cdot K] \underline{z} = P_{12} \cdot \underline{\omega}$$

$$\Rightarrow \underline{z} = [I - P_{11} \cdot K]^{-1} \cdot P_{12} \cdot \underline{\omega}$$

$$\Rightarrow \underline{u} = K \cdot [I - P_{11} \cdot K]^{-1} \cdot P_{12} \cdot \underline{\omega}$$

$$\Rightarrow \underline{y} = \left[ P_{22} + P_{21} \cdot K \cdot [I - P_{11} \cdot K]^{-1} \cdot P_{12} \right] \underline{\omega}$$

$$\Rightarrow f_u(P, K) = P_{22} + P_{21} \cdot K \cdot [I - P_{11} \cdot K]^{-1} \cdot P_{12}$$

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$f_u(P, K)$  is the upper linear fractional transform of  $P$  fed back by  $K$ .

National® Brand  
13-782 500 SHEETS FILLER 5" SQUARE  
42-391 50 SHEETS EASY-EASE 5" SQUARE  
42-389 100 SHEETS EASY-EASE 5" SQUARE  
42-392 100 RECYCLED WHITE 5" SQUARE  
42-399 200 RECYCLED WHITE 5" SQUARE  
Made in U.S.A.



In the time domain:

$$P(s) = \left[ \begin{array}{c|cc} A_P & B_{P1} & B_{P2} \\ \hline C_{P1} & D_{P11} & D_{P12} \\ C_{P2} & D_{P21} & D_{P22} \end{array} \right]$$

$$K(s) = \left[ \begin{array}{c|c} A_K & B_K \\ \hline C_K & D_K \end{array} \right]$$

$$\left| \begin{array}{l} \dot{X}_P = A_P X_P + B_{P1} U_1 + B_{P2} U_2 \\ U_1 = C_{P1} X_P + D_{P11} U_1 + D_{P12} U_2 \\ U_2 = C_{P2} X_P + D_{P21} U_1 + D_{P22} U_2 \\ \dot{X}_K = A_K X_K + B_K U \\ U = C_K X_K + D_K U \end{array} \right|$$

$$U = C_K X_K + D_K C_{P1} X_P + D_K D_{P11} U_1 + D_K D_{P12} U_2$$

$$\Rightarrow \underbrace{(I - D_K D_{P11})}_{DD} U = D_K C_{P1} X_P + C_K X_K + D_K D_{P12} U$$

$$\Rightarrow U = DD^T D_K C_{P1} X_P + DD^T C_K X_K + DD^T D_K D_{P12} U$$



$$\dot{x}_P = [A_P + B_{P_1} \cdot D\bar{D}^{-1} D_K C_{P_1}] x_P + [B_{P_1} \cdot D\bar{D}^{-1} C_K] x_K \\ + [B_{P_2} + B_{P_1} \cdot D\bar{D}^{-1} D_K D_{P_{12}}] \underline{\omega}$$

$$\dot{x}_K = [B_K C_{P_1}] x_P + A_K x_K + [B_K D_{P_{12}}] \underline{\epsilon} + [B_K D_{P_{11}}] \underline{\epsilon}$$

$$\Rightarrow \dot{x}_K = [B_K C_{P_1} + B_K D_{P_{11}} \cdot D\bar{D}^{-1} D_K C_{P_1}] x_P \\ + [A_K + B_K D_{P_{11}} \cdot D\bar{D}^{-1} C_K] x_K \\ + [B_K D_{P_{12}} + B_K D_{P_{11}} \cdot D\bar{D}^{-1} D_K D_{P_{12}}] \underline{\epsilon}$$

$$y = [C_{P_2} + D_{P_{21}} \cdot D\bar{D}^{-1} D_K C_{P_1}] x_P + [D_{P_{21}} \cdot D\bar{D}^{-1} C_K] x_K \\ + [D_{P_{22}} + D_{P_{21}} \cdot D\bar{D}^{-1} D_K D_{P_{12}}] \underline{\epsilon}$$

$$\Rightarrow f_u(P, K) = \frac{\begin{bmatrix} (A_P + B_P \cdot D\bar{D}^{-1} D_K C_{P_1}) & (B_P \cdot D\bar{D}^{-1} C_K) \\ (B_K C_{P_1} + B_K D_{P_{11}} \cdot D\bar{D}^{-1} D_K C_{P_1}) & (A_K + B_K D_{P_{11}} \cdot D\bar{D}^{-1} C_K) \end{bmatrix}}{\begin{bmatrix} (C_{P_2} + D_{P_{21}} \cdot D\bar{D}^{-1} D_K C_{P_1}) & (D_{P_{21}} \cdot D\bar{D}^{-1} C_K) \\ (B_{P_2} + B_{P_1} \cdot D\bar{D}^{-1} D_K D_{P_{12}}) & (B_K D_{P_{12}} + B_K D_{P_{11}} \cdot D\bar{D}^{-1} D_K D_{P_{12}}) \end{bmatrix}} \\ \frac{(D_{P_{22}} + D_{P_{21}} \cdot D\bar{D}^{-1} D_K D_{P_{12}})}{.}$$

13-782 500 SHEETS, FILLER, 5" SQUARE  
42-381 50 SHEETS EYE LASER PAPER, SQUARE  
42-382 100 SHEETS EYE LASER PAPER, SQUARE  
42-383 100 RECYCLED WHITE, 5" SQUARE  
42-384 200 RECYCLED WHITE, 5" SQUARE  
42-389 200 RECYCLED WHITE, 5" SQUARE  
NCR corp. U.S.A.



$$P_p(s) \cdot \underline{x}_p(t) = Q_{P_1}(s) \cdot \underline{u}(t) + Q_{P_2}(s) \cdot \underline{w}(t)$$

$$\underline{z}(t) = R_{P_1}(s) \cdot \underline{x}_p(t) + W_{P_{11}}(s) \cdot \underline{u}(t) + W_{P_{12}}(s) \cdot \underline{w}(t)$$

$$\underline{y}(t) = R_{P_2}(s) \cdot \underline{x}_p(t) + W_{P_{21}}(s) \cdot \underline{u}(t) + W_{P_{22}}(s) \cdot \underline{w}(t)$$

$$P_k(s) \cdot \underline{x}_k(s) = Q_k(s) \cdot \underline{z}(t)$$

$$\underline{u}(t) = R_k(s) \cdot \underline{x}_k(t) + W_k(s) \cdot \underline{z}(t)$$

$$\Rightarrow P_p(s) \cdot \underline{x}_p(t) - Q_{P_1} \cdot \underline{u}(t) = Q_{P_2}(s) \cdot \underline{w}(t)$$

$$P_k(s) \cdot \underline{x}_k(t) - Q_k(s) \cdot \underline{z}(t) = \emptyset$$

$$-R_k(s) \cdot \underline{x}_k(t) - W_k(s) \cdot \underline{z}(t) + \underline{u}(t) = \emptyset$$

$$-R_{P_1}(s) \cdot \underline{x}_p(t) + \underline{z}(t) - W_{P_{11}}(s) \cdot \underline{u}(t) = W_{P_{12}}(s) \cdot \underline{w}(t)$$

$$\underline{y}(t) = R_{P_2}(s) \cdot \underline{x}_p(t) + W_{P_{21}}(s) \cdot \underline{u}(t) + W_{P_{22}}(s) \cdot \underline{w}(t)$$

Let:  $\underline{m} = \begin{bmatrix} \underline{x}_p(t) \\ \underline{x}_k(t) \\ -\underline{z}(t) \\ -\underline{u}(t) \end{bmatrix}$

National® Brand  
13-782 50 SHEETS FILLER 5 SQUARE  
42-381 100 SHEETS EYE-EASE® 5 SQUARE  
42-382 200 SHEETS EYE-EASE® 5 SQUARE  
42-383 200 RECYCLED WHITE 5 SQUARE  
42-389 200 RECYCLED WHITE 5 SQUARE  
Made in U.S.A.

$\Rightarrow$

$$\begin{bmatrix} P_p(s) & \emptyset & \emptyset & Q_{P_1}(s) \\ \emptyset & P_k(s) & Q_k(s) & \emptyset \\ \emptyset & -R_k(s) & W_k(s) & -I \\ -R_{P_1}(s) & \emptyset & -I & W_{P_{12}}(s) \end{bmatrix} \underline{\underline{m}}(t) = \begin{bmatrix} Q_{P_2}(s) \\ \emptyset \\ \emptyset \\ W_{P_{22}}(s) \end{bmatrix} w(t)$$

$$y(t) = [R_{P_2}(s) \ \emptyset \ \emptyset \ -W_{P_{21}}(s)] \underline{\underline{m}}(t) + [W_{P_{22}}(s)] w(t)$$

is a polynomial matrix system  
representation of  $\tilde{f}_u(P, K)$ .

500 SHEETS FILLER'S SQUARE  
50 SHEETS EASY-ERASE  
100 SHEETS EASY-ERASE  
200 SHEETS EASY-ERASE  
100 RECYCLED WHITE 5 SQUARE  
42-392 42-399 200 RECYCLED WHITE 5 SQUARE  
Made in S.A.

